

SCHEMA O SOLUZIONE QUALITATIVA

REAZIONI VINCOLARI

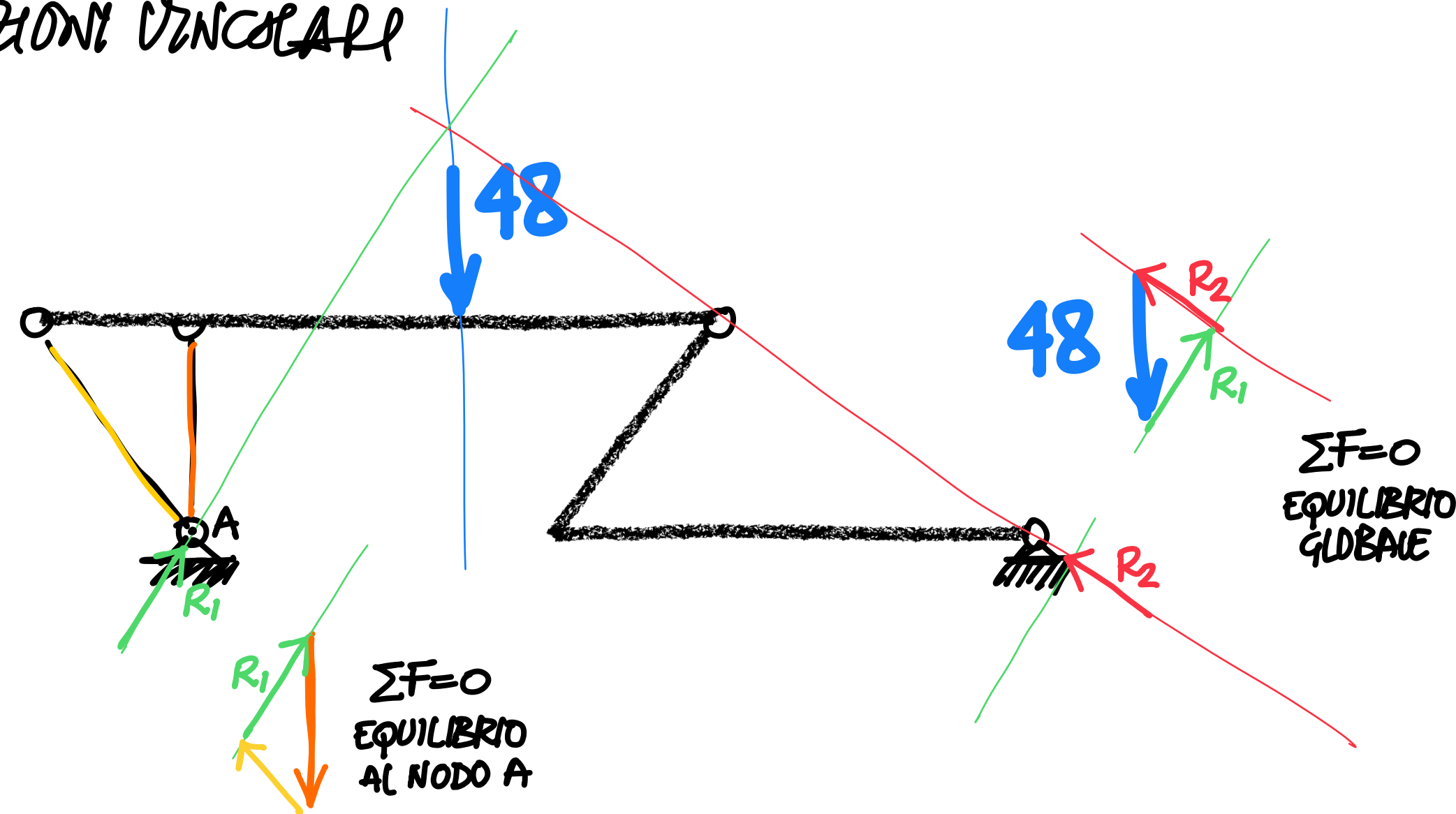
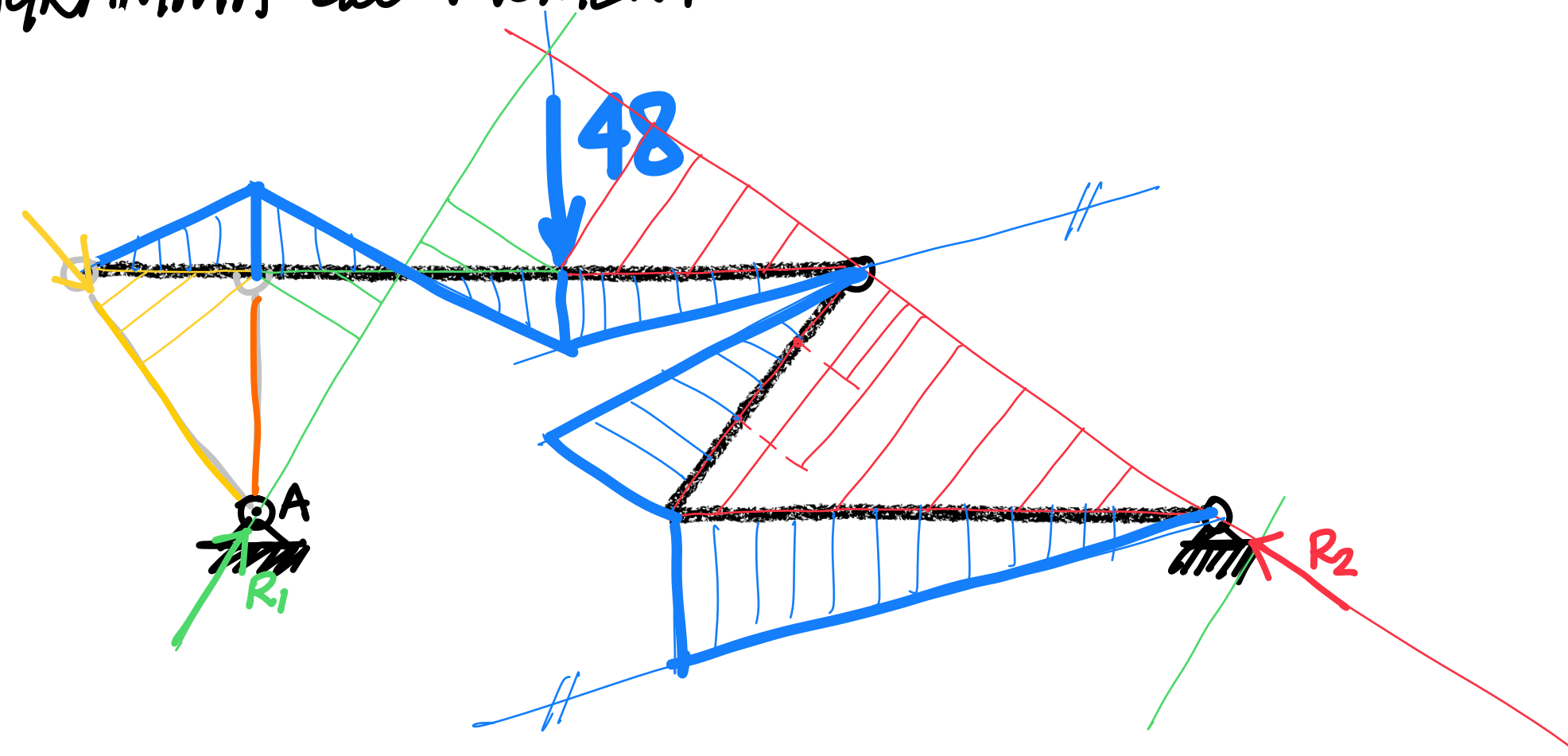


DIAGRAMMA del MOMENTO



SCHEMA X SOLUZIONE QUALITATIVA

REAZIONI VINCOLARI

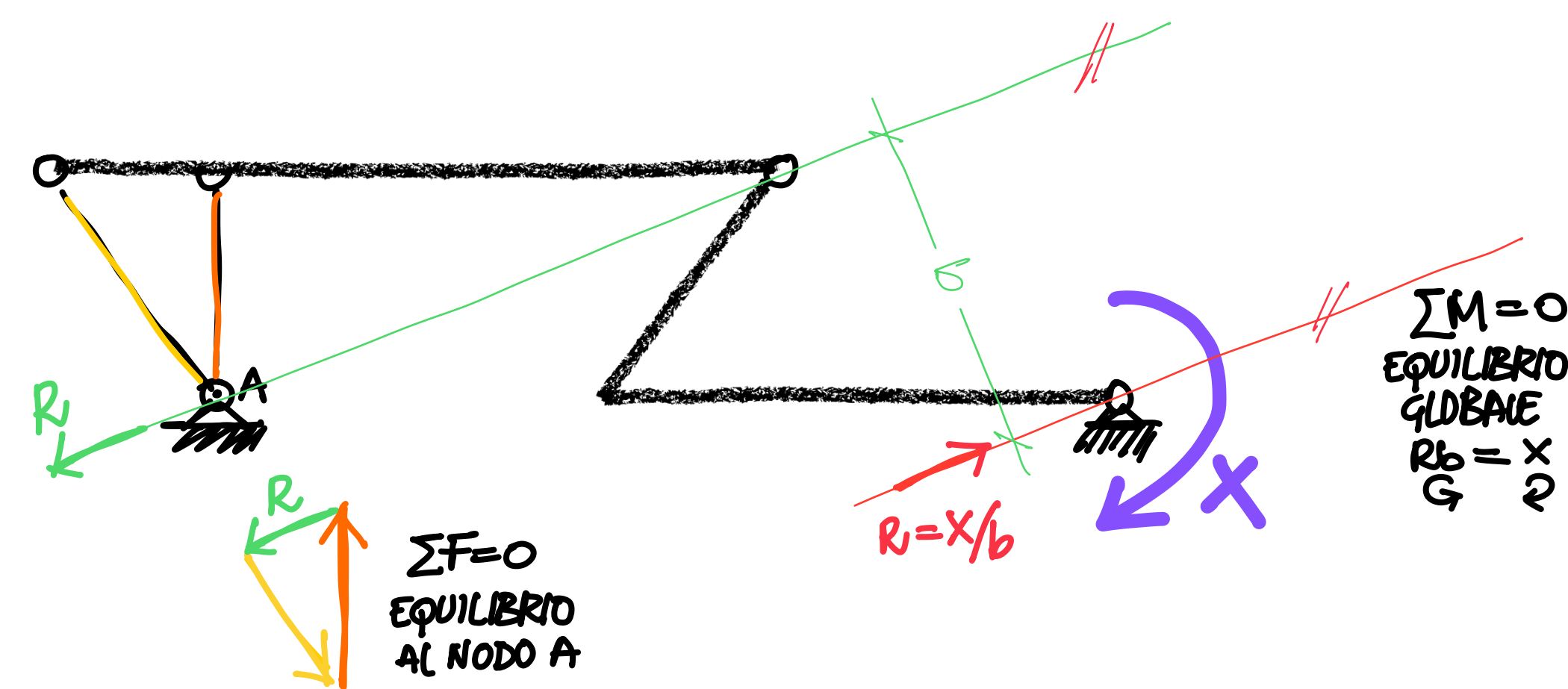
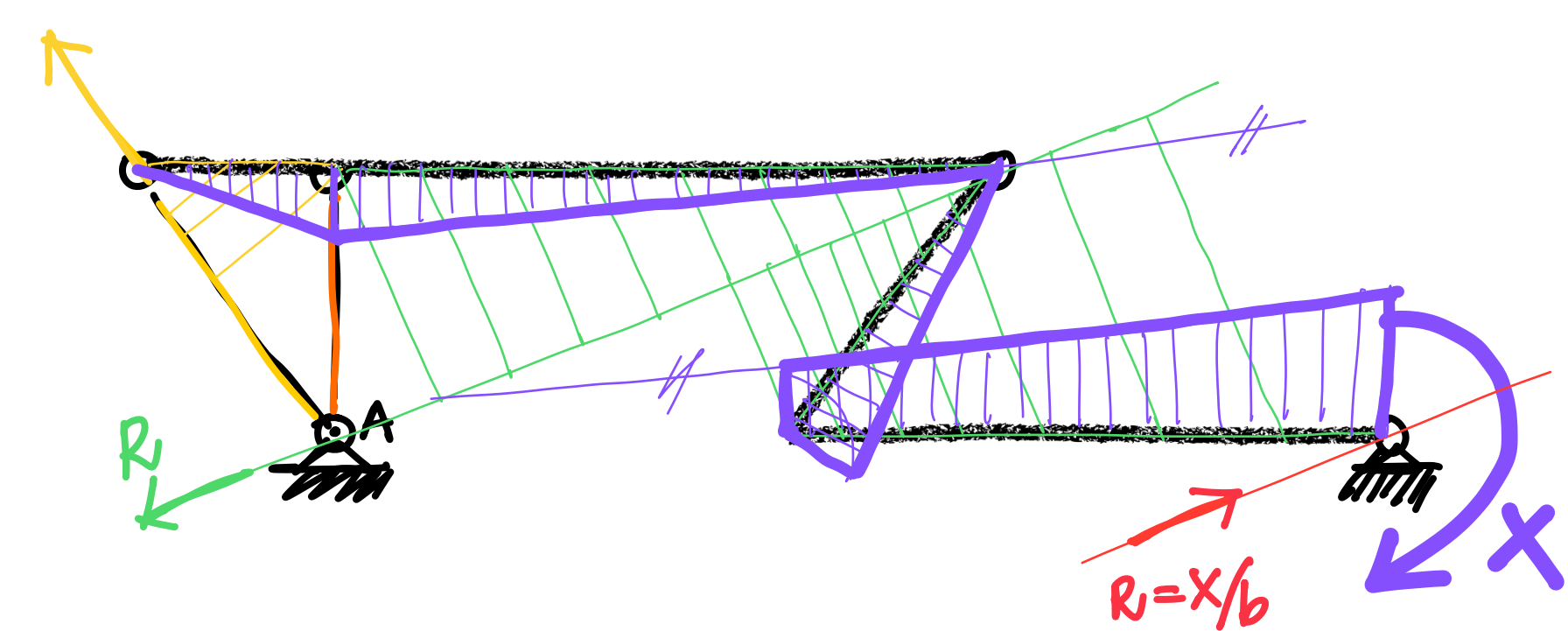
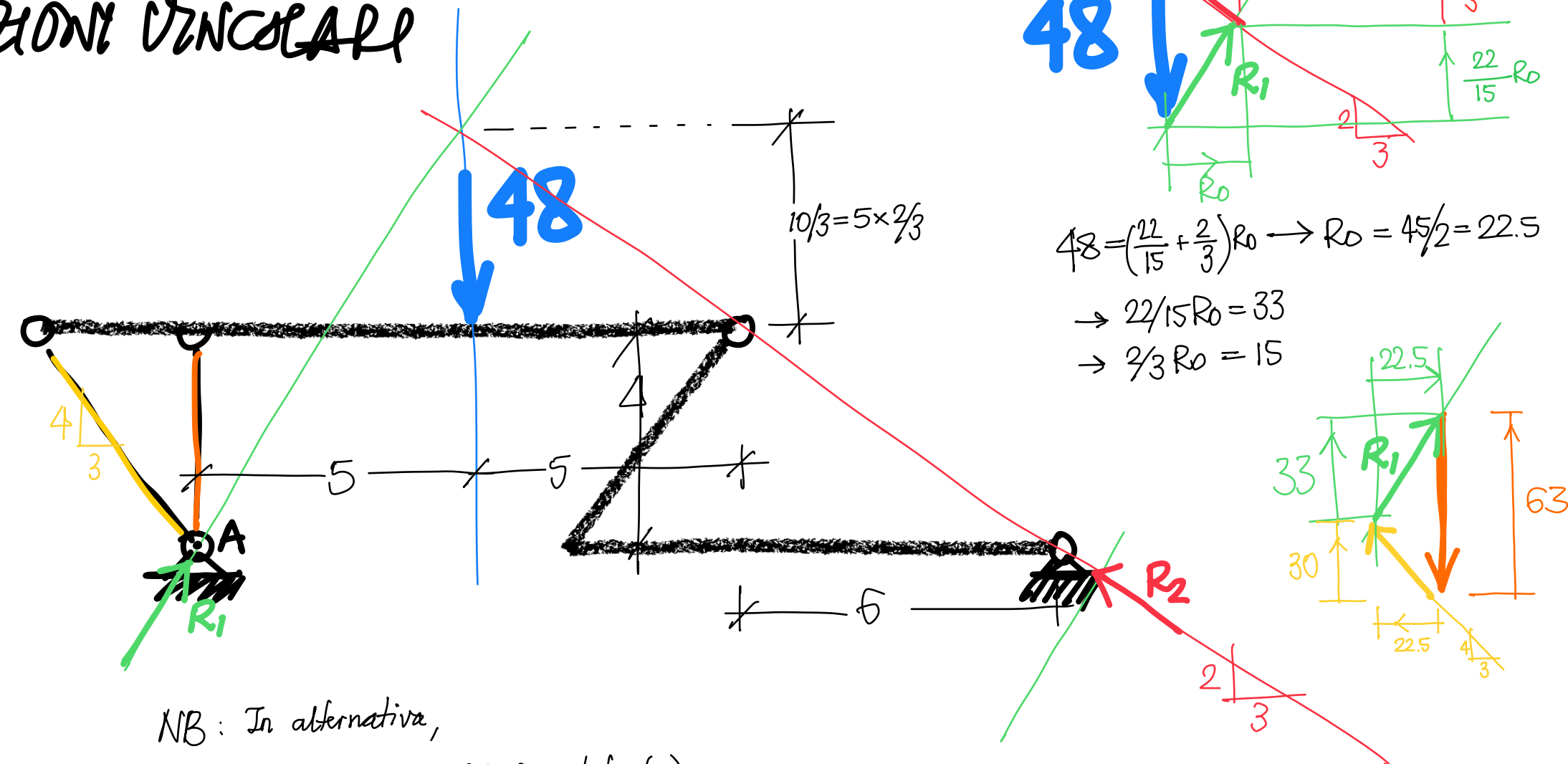


DIAGRAMMA del MOMENTO



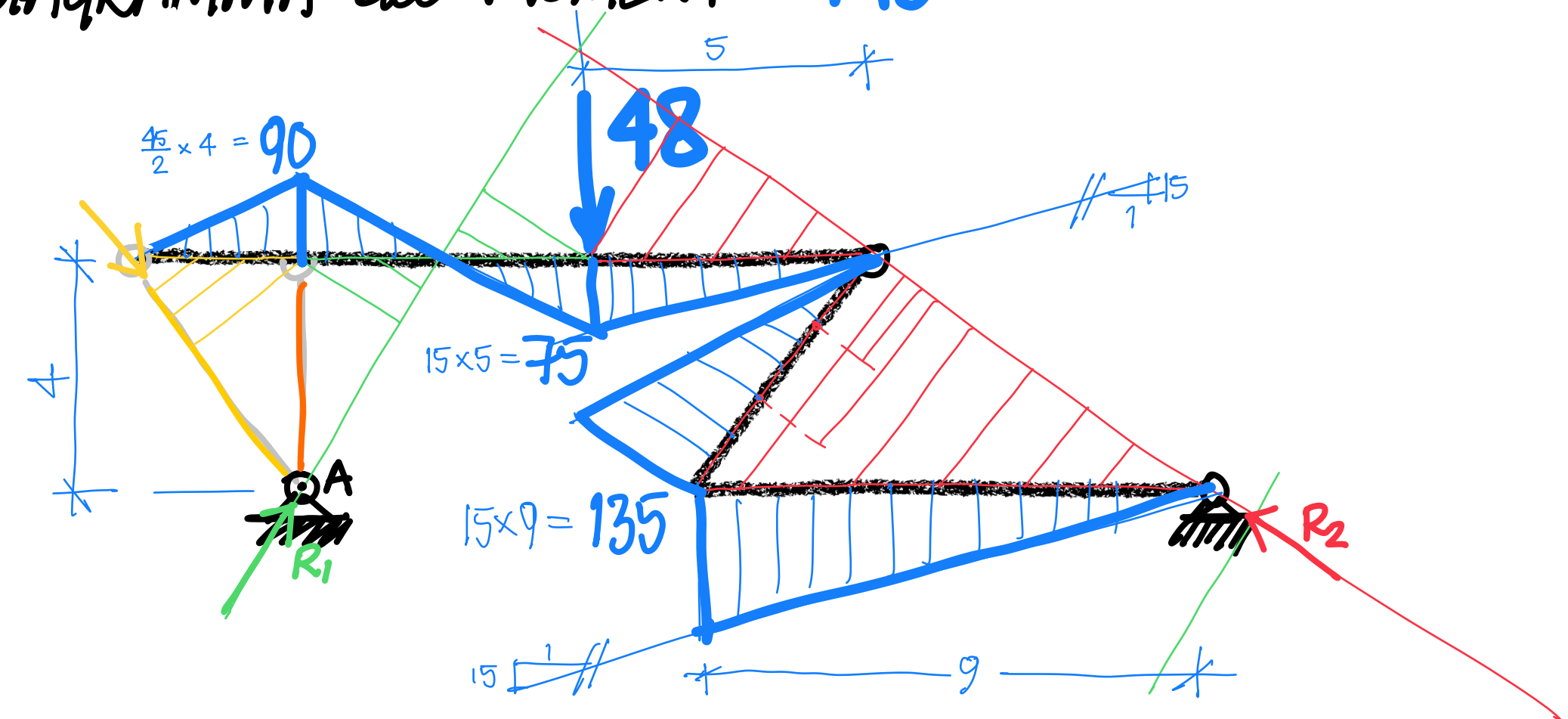
SCHEMA O SOLUZIONE QUANTITATIVA

REAZIONI VINCOLARI



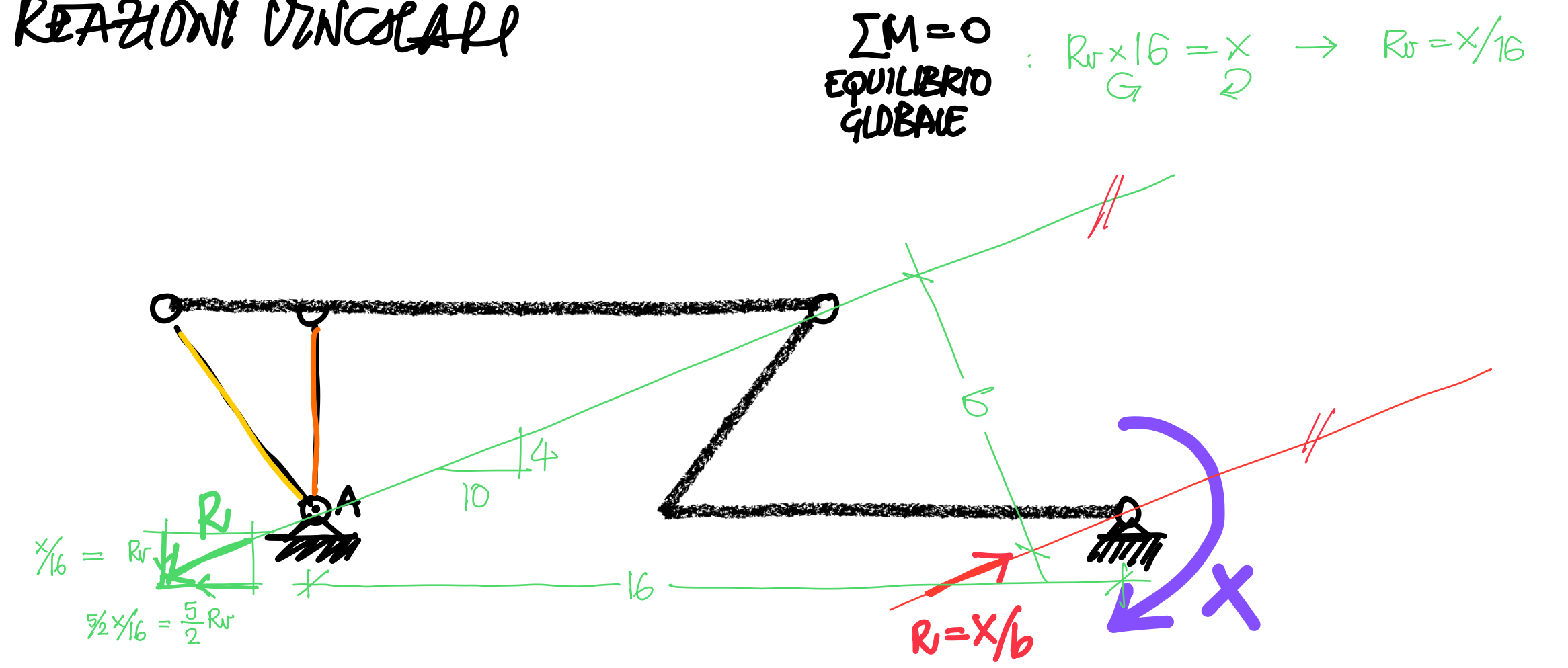
NB: In alternativa,
 $\sum M = 0$ (equilibrio globale)
 $\overset{A}{\curvearrowright} R_2 \times 16 = 48 \times 5 \rightarrow R_2 = 15$
 \curvearrowright

DIAGRAMMA del MOMENTO M_0



SCHEMA X SOLUZIONE QUANTITATIVA

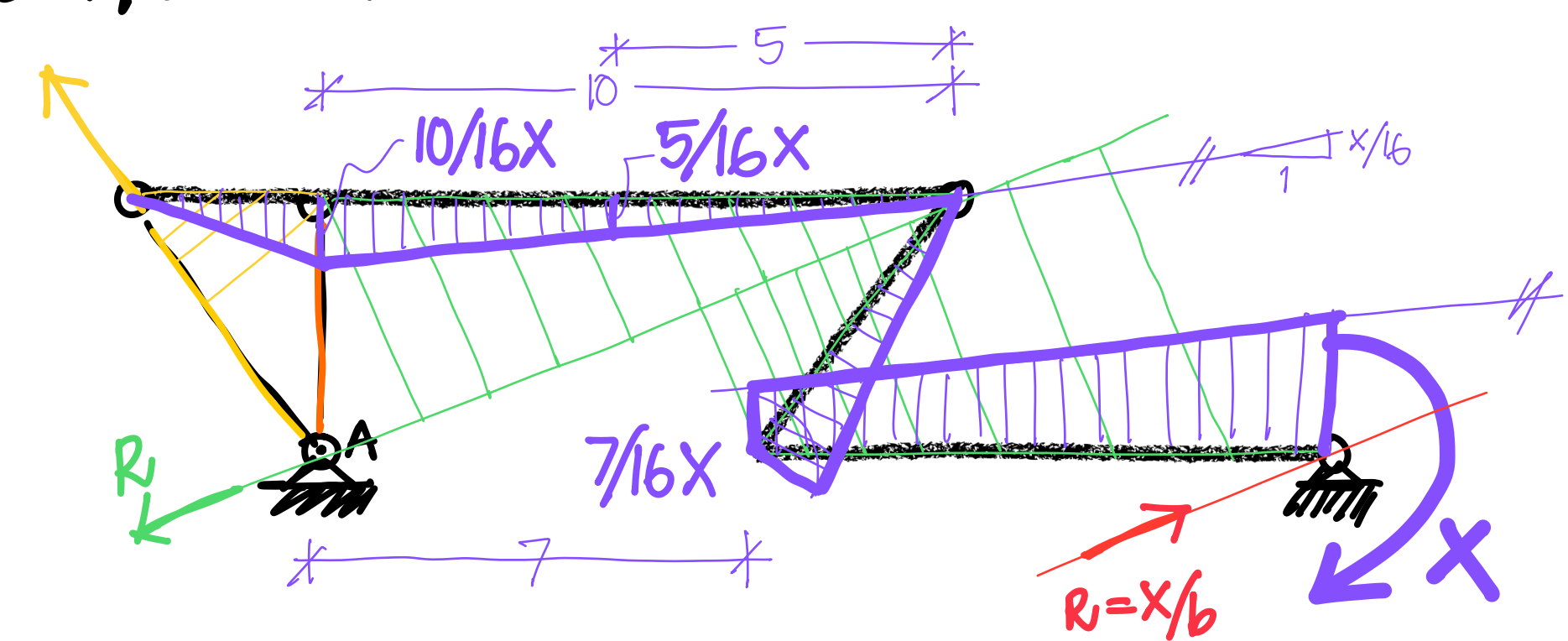
REAZIONI VINCOLARI



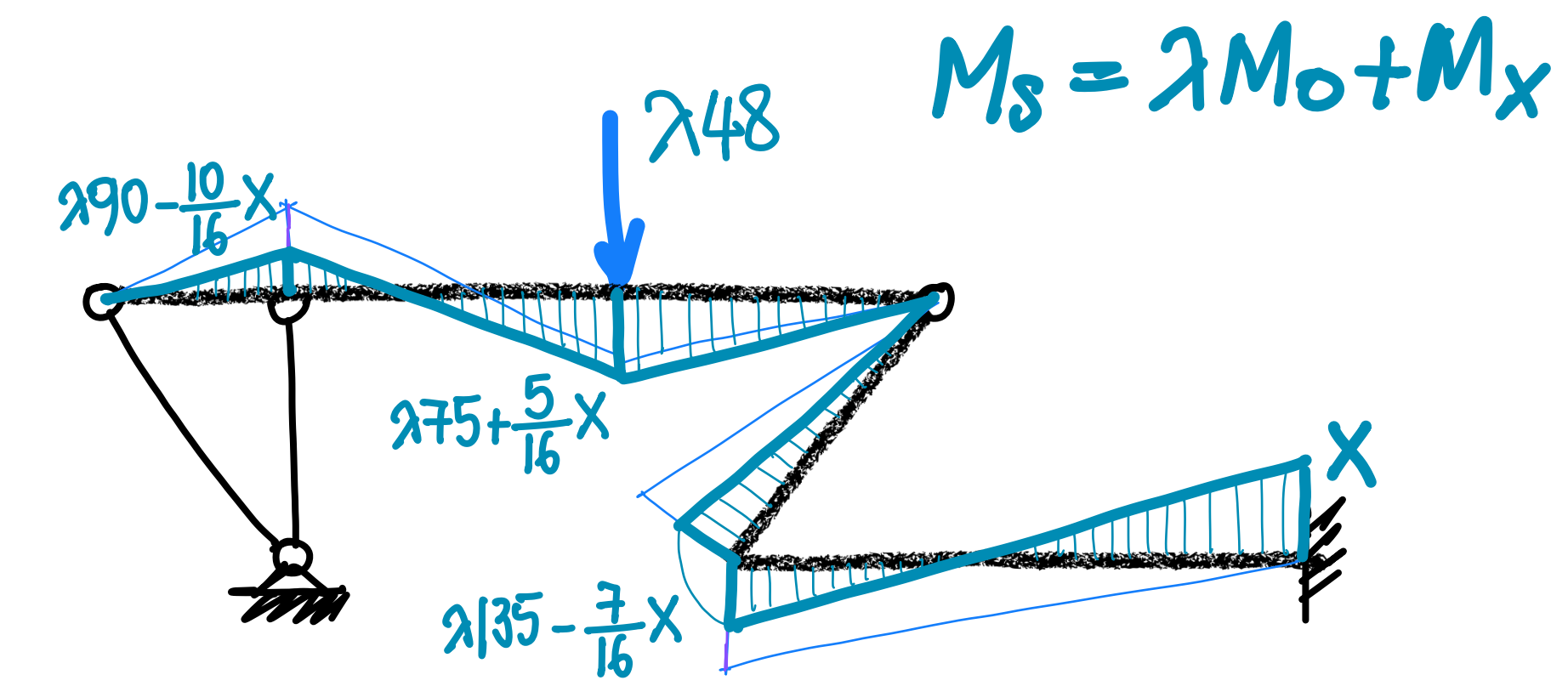
$\sum M = 0$
EQUILIBRIO GLOBALE
 $R_2 \times 16 = X \times 10 \rightarrow R_2 = X/6$

$\sum F = 0$
EQUILIBRIO AL NODO A
 $\frac{4.5}{3} \times \frac{X}{16} = \frac{10}{16} \times \frac{X}{16}$

DIAGRAMMA del MOMENTO M_x

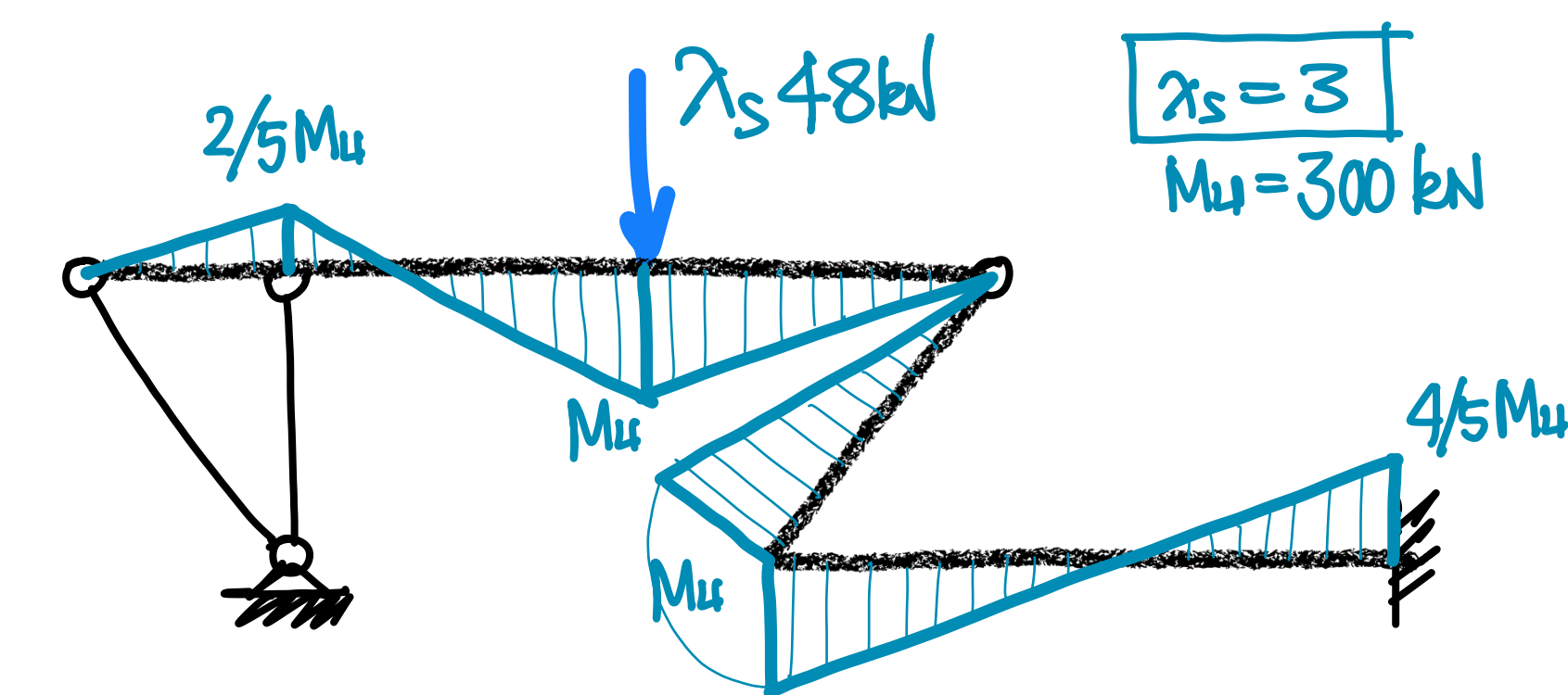


APPROCCIO STATICO



* ipotesi 1: $x=0$
 $\rightarrow \lambda_s 135 = M_u = 300 \rightarrow \lambda_s = 300/135 = 20/9 \simeq 2.22$

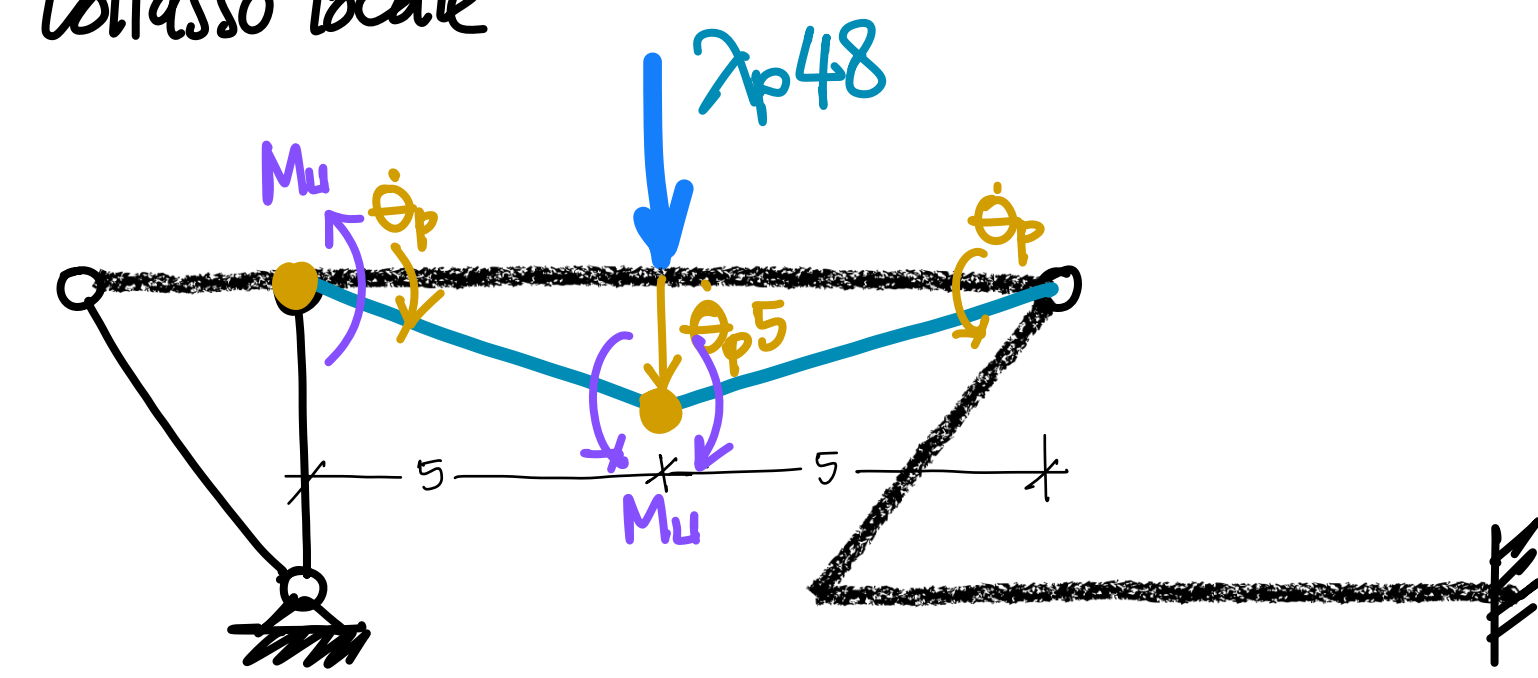
* ipotesi 2: $x \neq 0$
 $\rightarrow \begin{cases} \lambda_s 75 + 5/16 x = M_u \\ \lambda_s 135 - 7/16 x = M_u \end{cases} \rightarrow \boxed{\lambda_s = 3} \quad (x = 240 = 4/5 M_u)$
verifica: $\lambda_s 90 - 10/16 x = 120 = 2/5 M_u < M_u$



$$\boxed{\lambda_s = \lambda_p = 3 = \lambda_c}$$

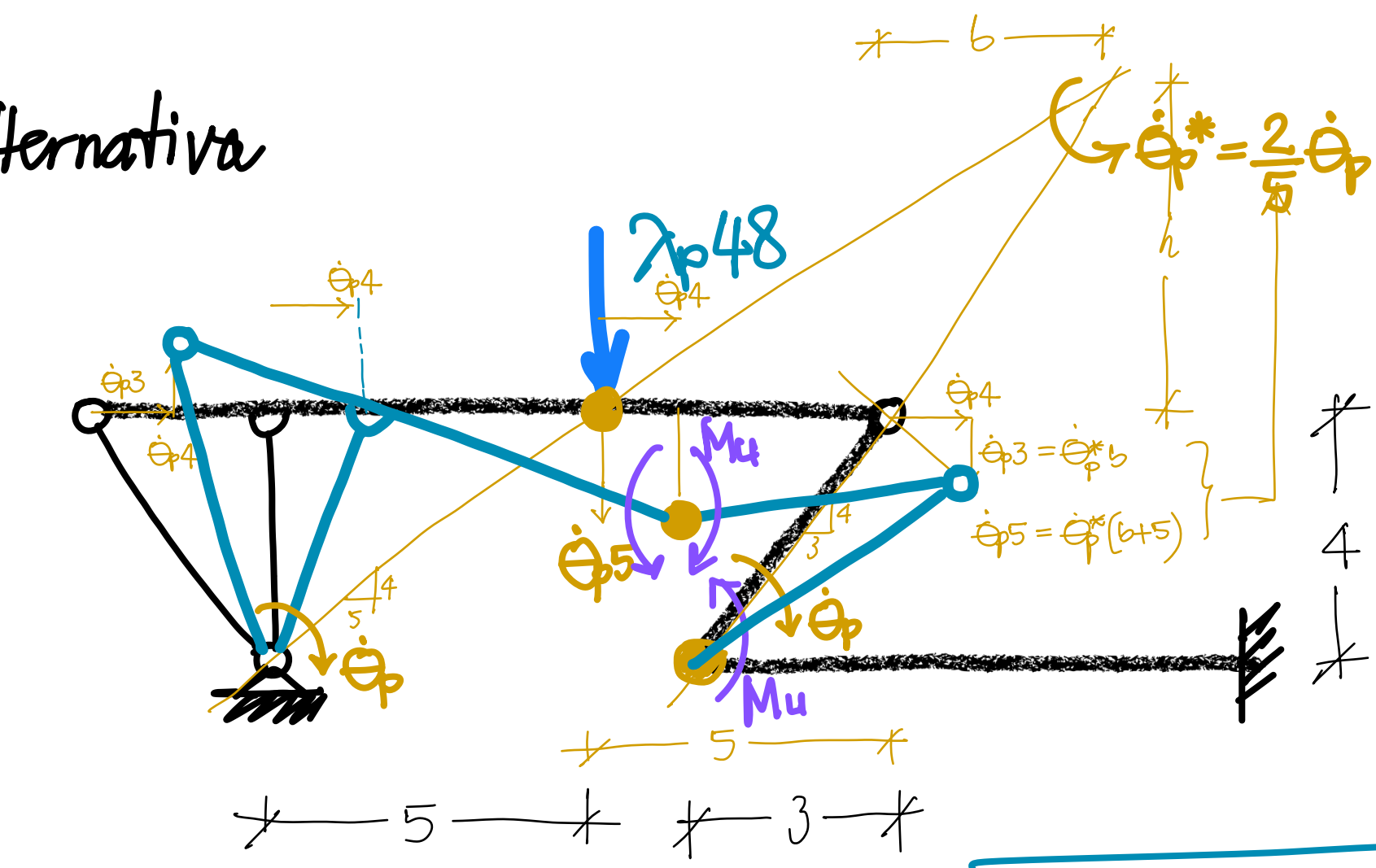
APPROCCIO CINEMATICO

* ipotesi di collasso locale



$$\dot{Q} = \lambda_p 48 \dot{\theta}_p 5 - (M_u \dot{\theta}_p + M_u 2 \dot{\theta}_p) = 0 \rightarrow \lambda_p = \frac{M_u 3 \dot{\theta}_p}{48 \dot{\theta}_p 5} = 3.75$$

* ipotesi alternativa



$$\dot{Q} = \lambda_p 48 \dot{\theta}_p 5 - (M_u \dot{\theta}_p + M_u (\dot{\theta}_p + \frac{2}{5} \dot{\theta}_p)) = 0 \rightarrow \boxed{\lambda_p = \frac{M_u 12/5 \dot{\theta}_p}{48 \dot{\theta}_p 5} = 3}$$

SCHEMA O

DIAGRAMMA N₀

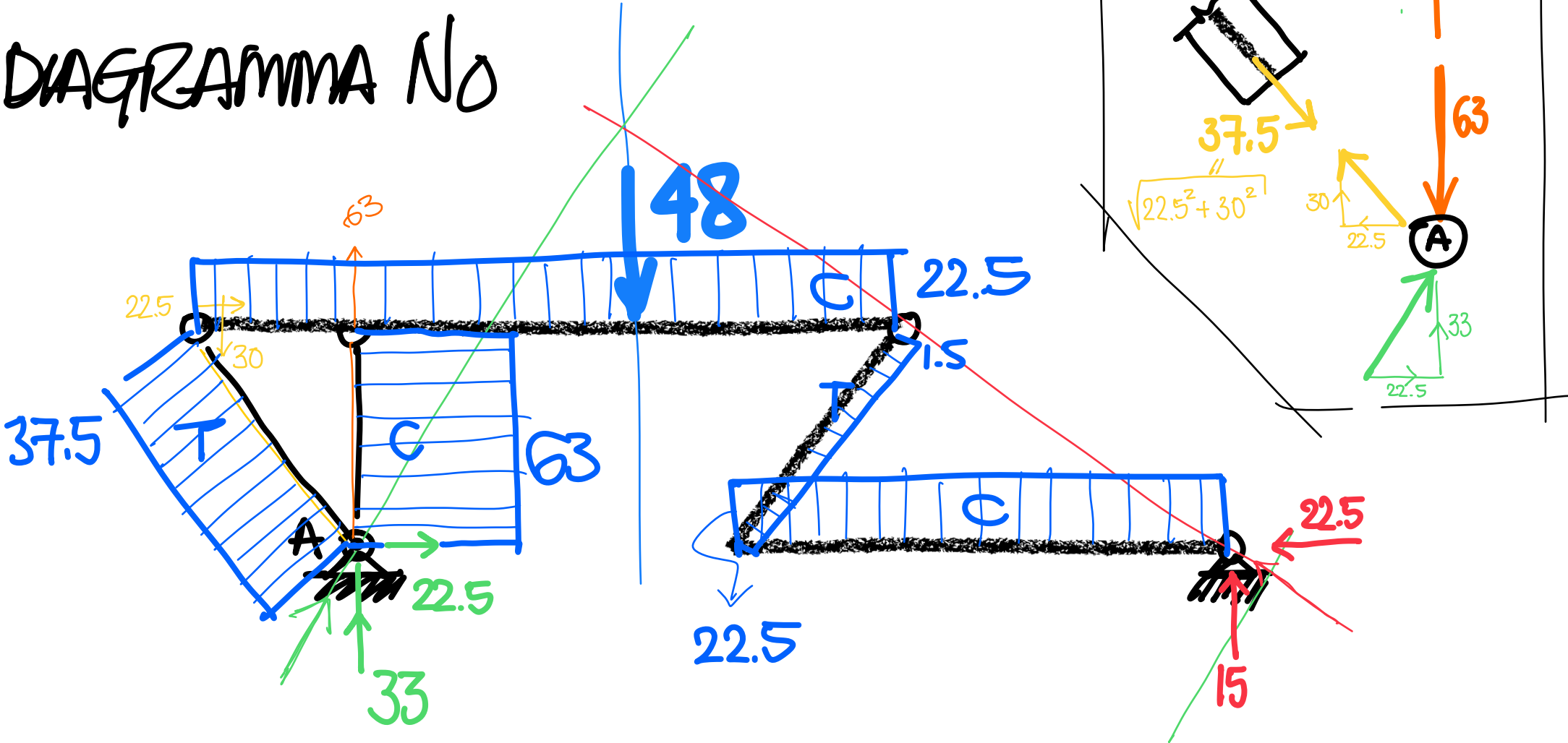
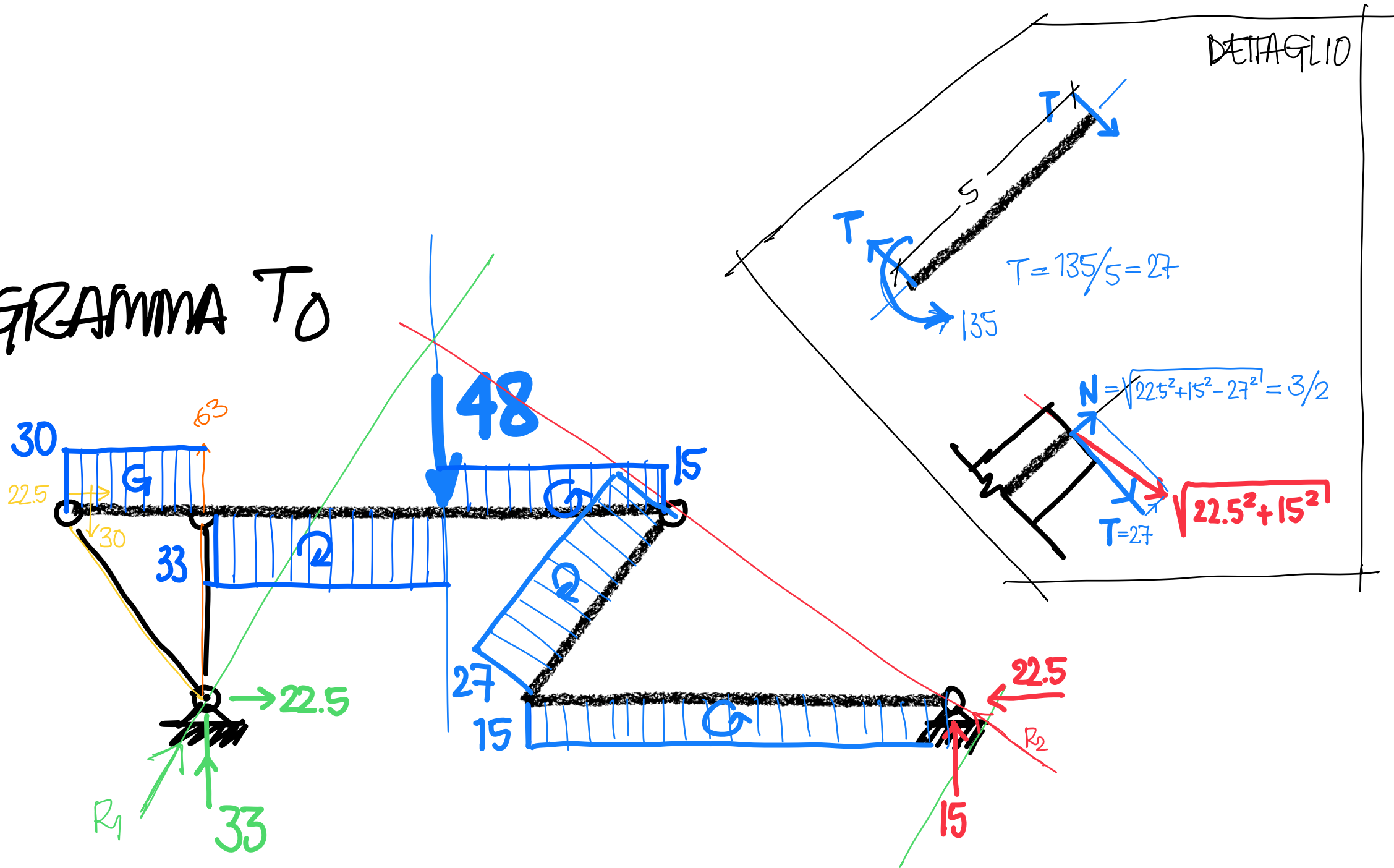


DIAGRAMMA T₀



SCHEMA X

DIAGRAMMA N_x

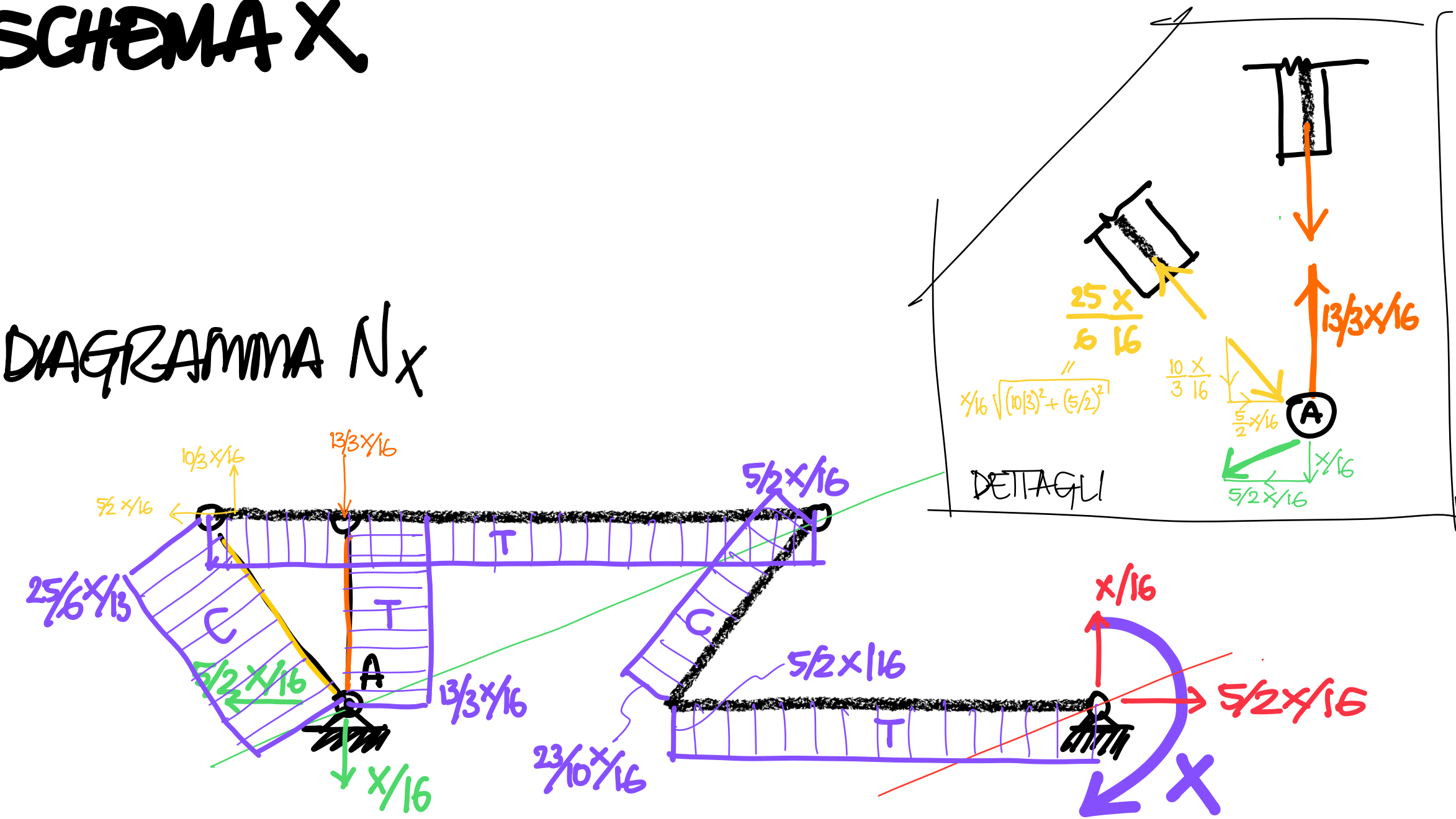


DIAGRAMMA T_x

