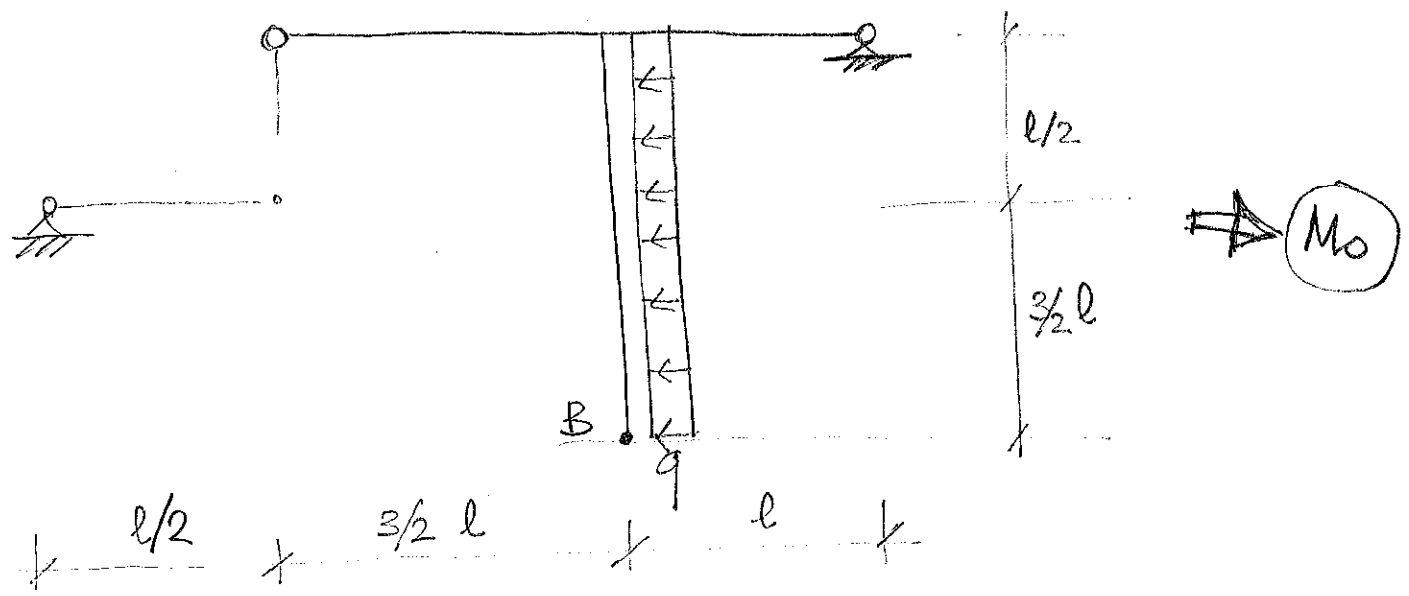
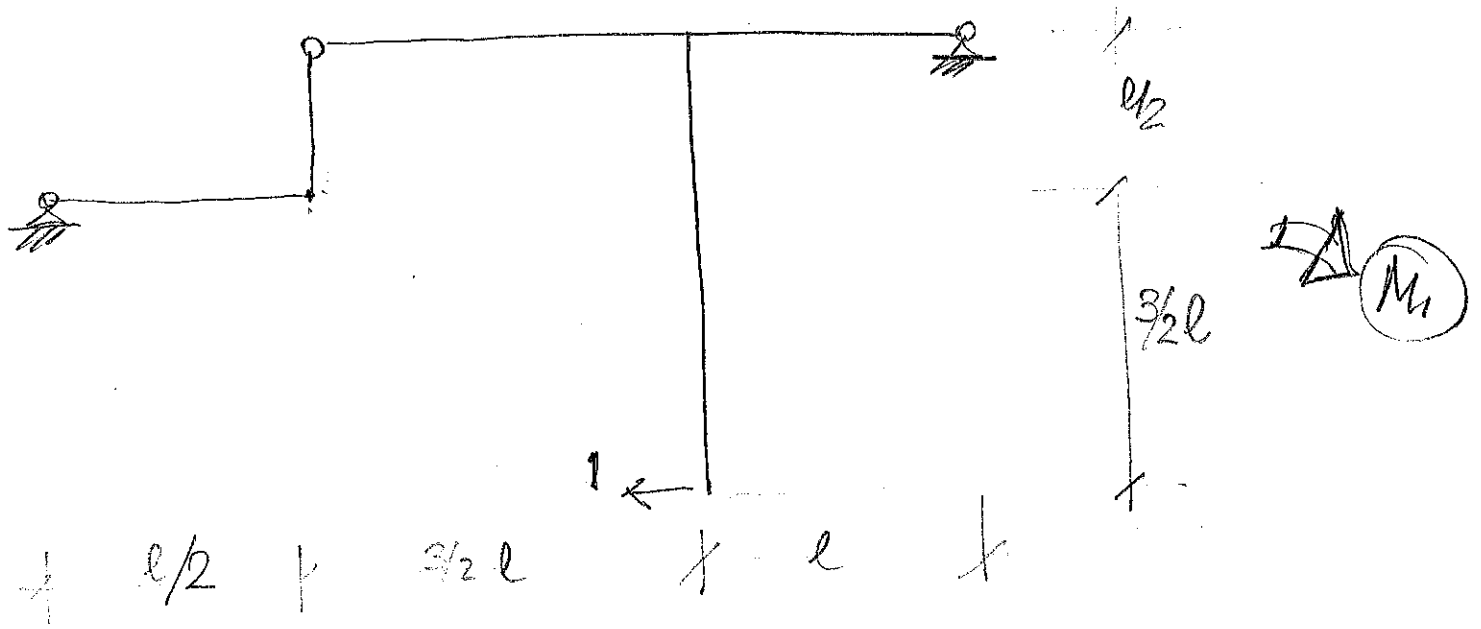


ESEMPIO

calcolo sullo spostamento orizzontale in B con il metodo delle forze



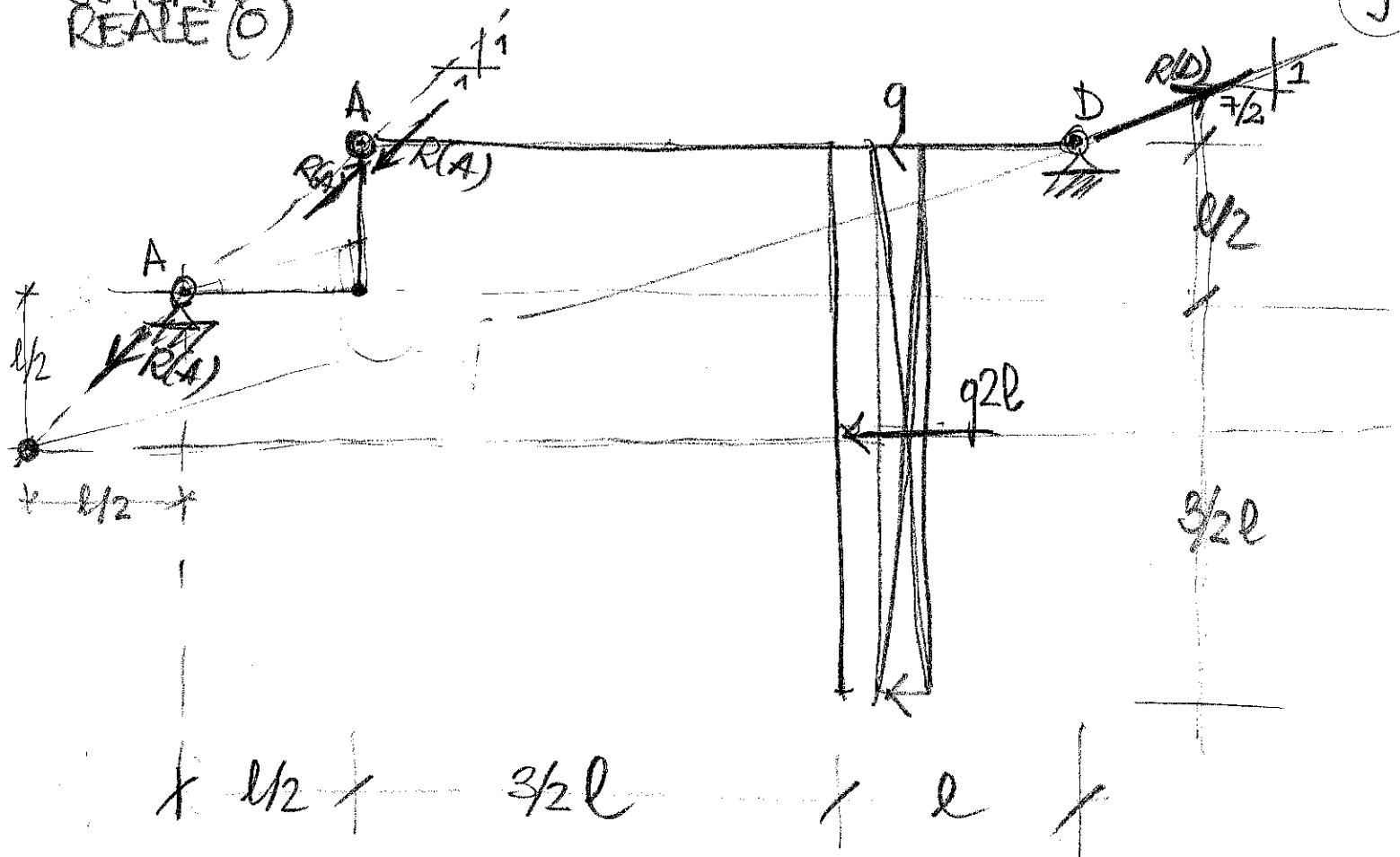
si aggiunge uno schema virtuale con forza unitaria orizzontale in B



I due momenti M_0, M_1 relativi ai due schemi sono risolti per via grafica.

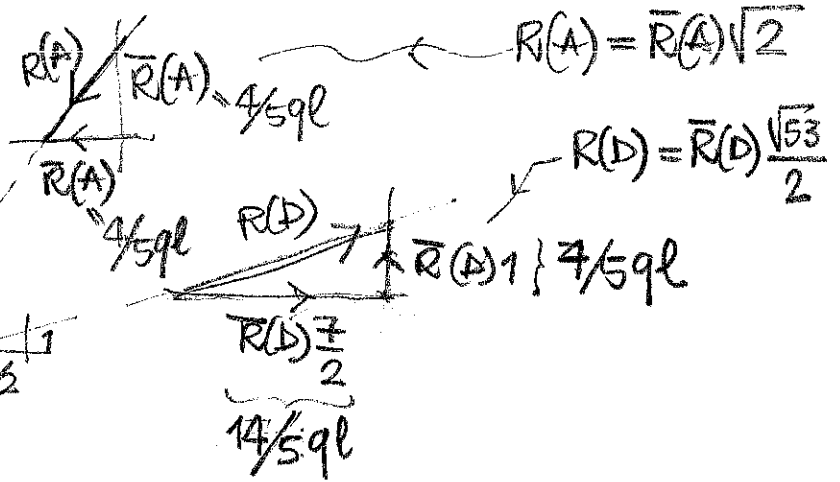
SCHEMA
REALE (0)

(9)



EQL. RISULTANTI

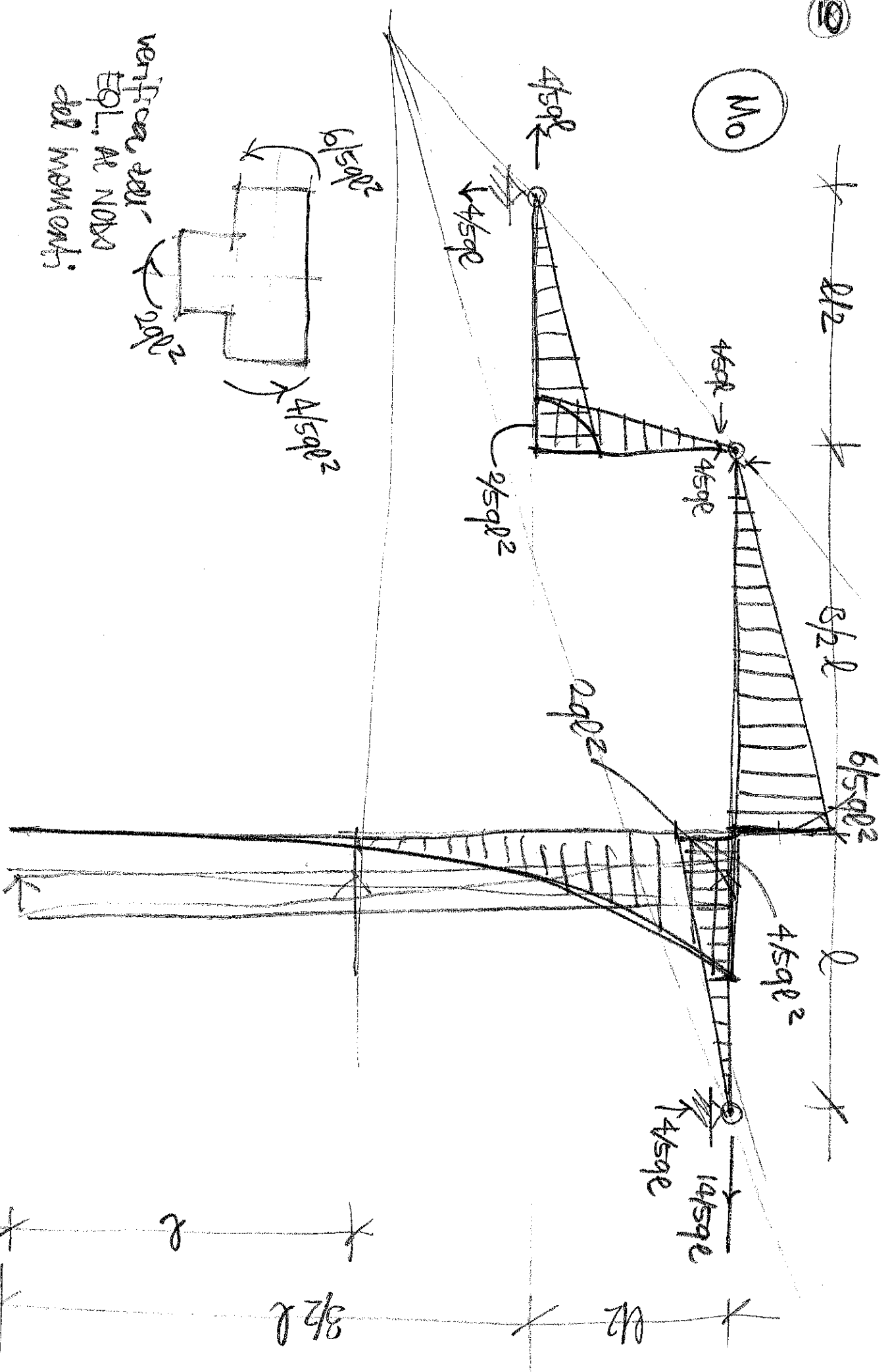
$$\begin{cases} \bar{R}(A) + 2ql = \frac{7}{2} \bar{R}(D) \\ \bar{R}(D) = \bar{R}(A) \end{cases}$$



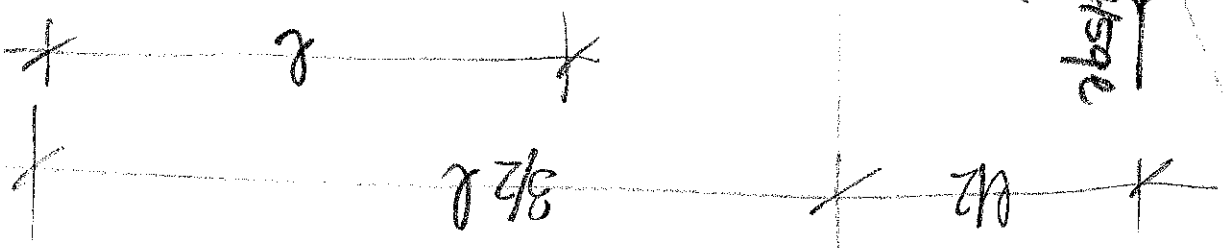
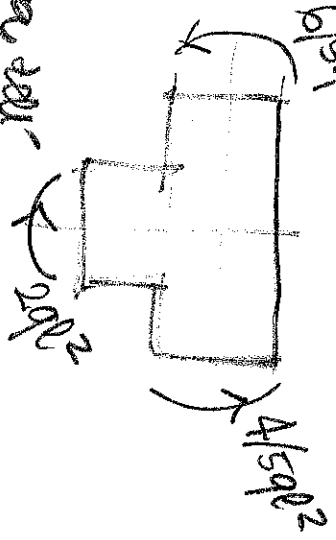
$$\begin{cases} \bar{R}(D) = \frac{4}{5} ql \\ \bar{R}(A) = \frac{4}{5} ql \end{cases}$$

②

M₀



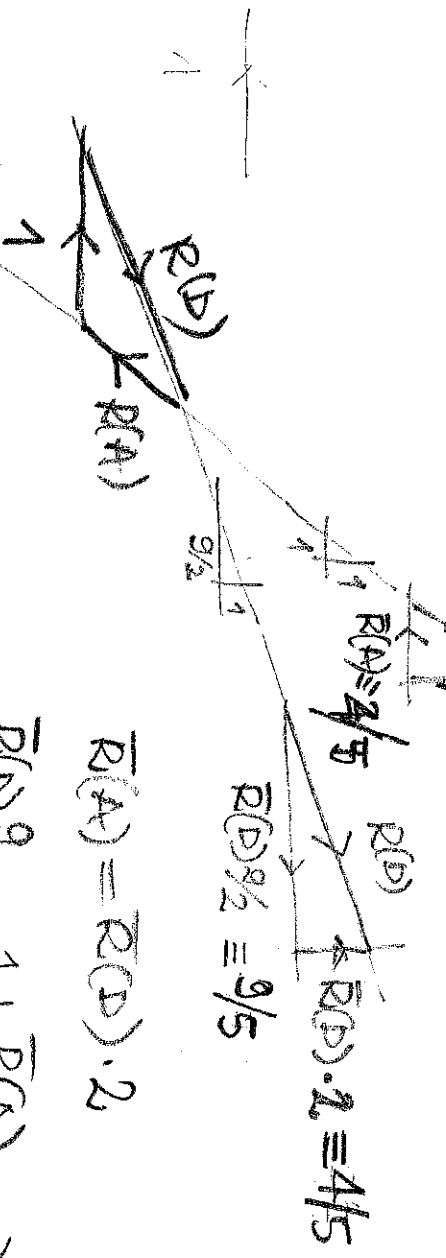
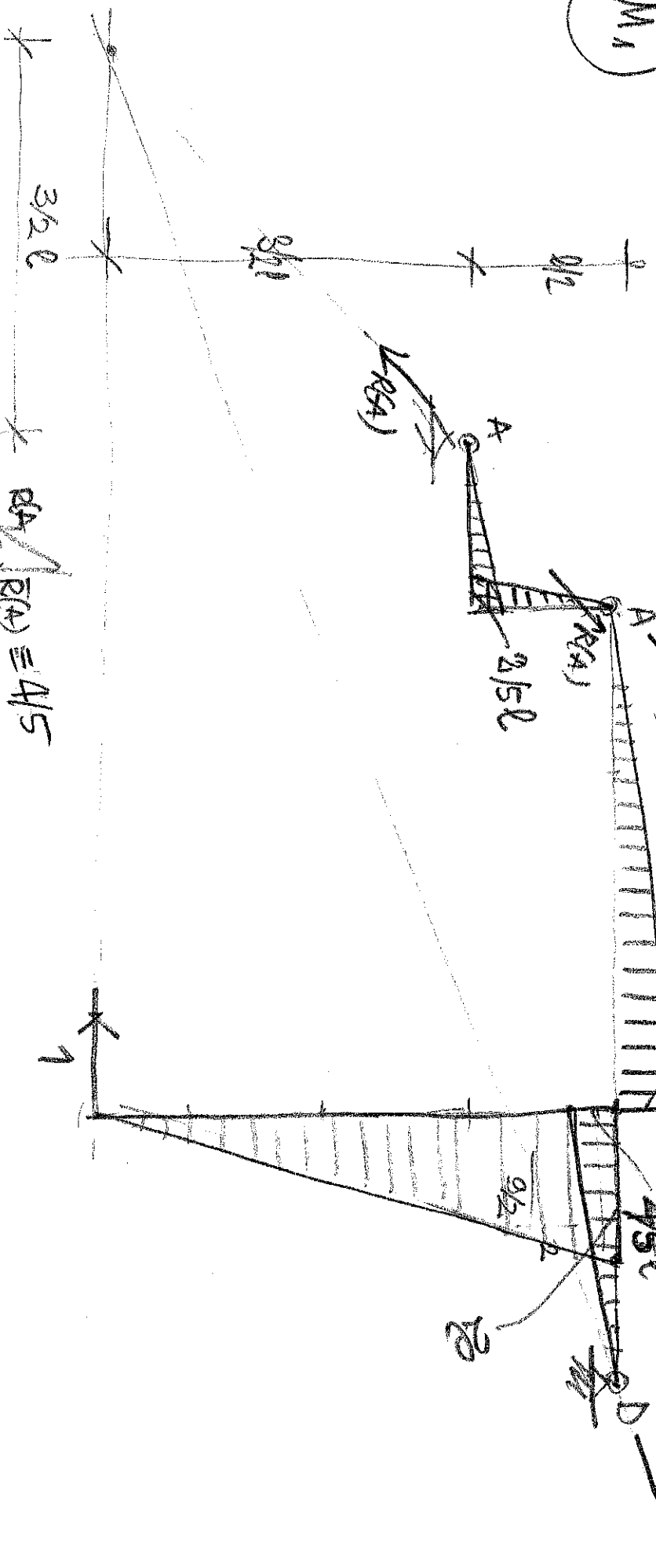
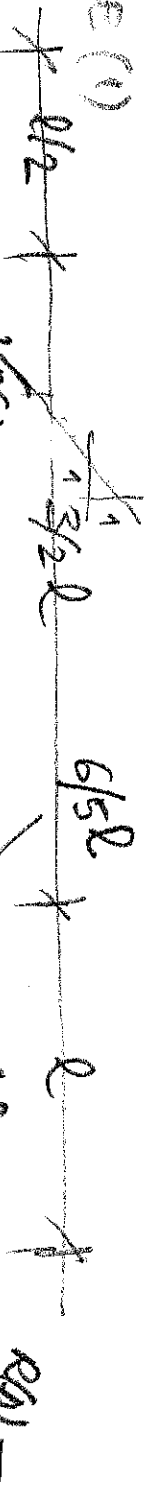
vertical axis
EQL. AC NOVA
for moments



5

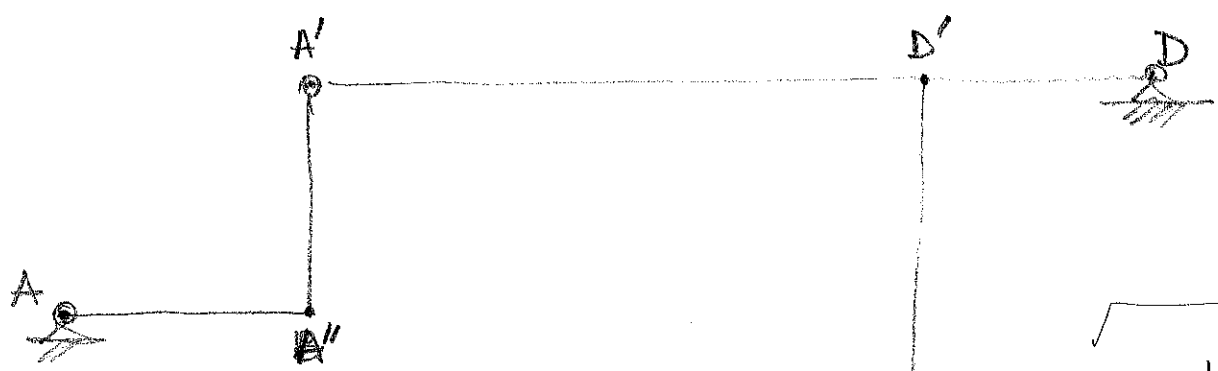
M_1

SHEAR FORCE (V)



$$R(A) = R(D) \cdot 2$$

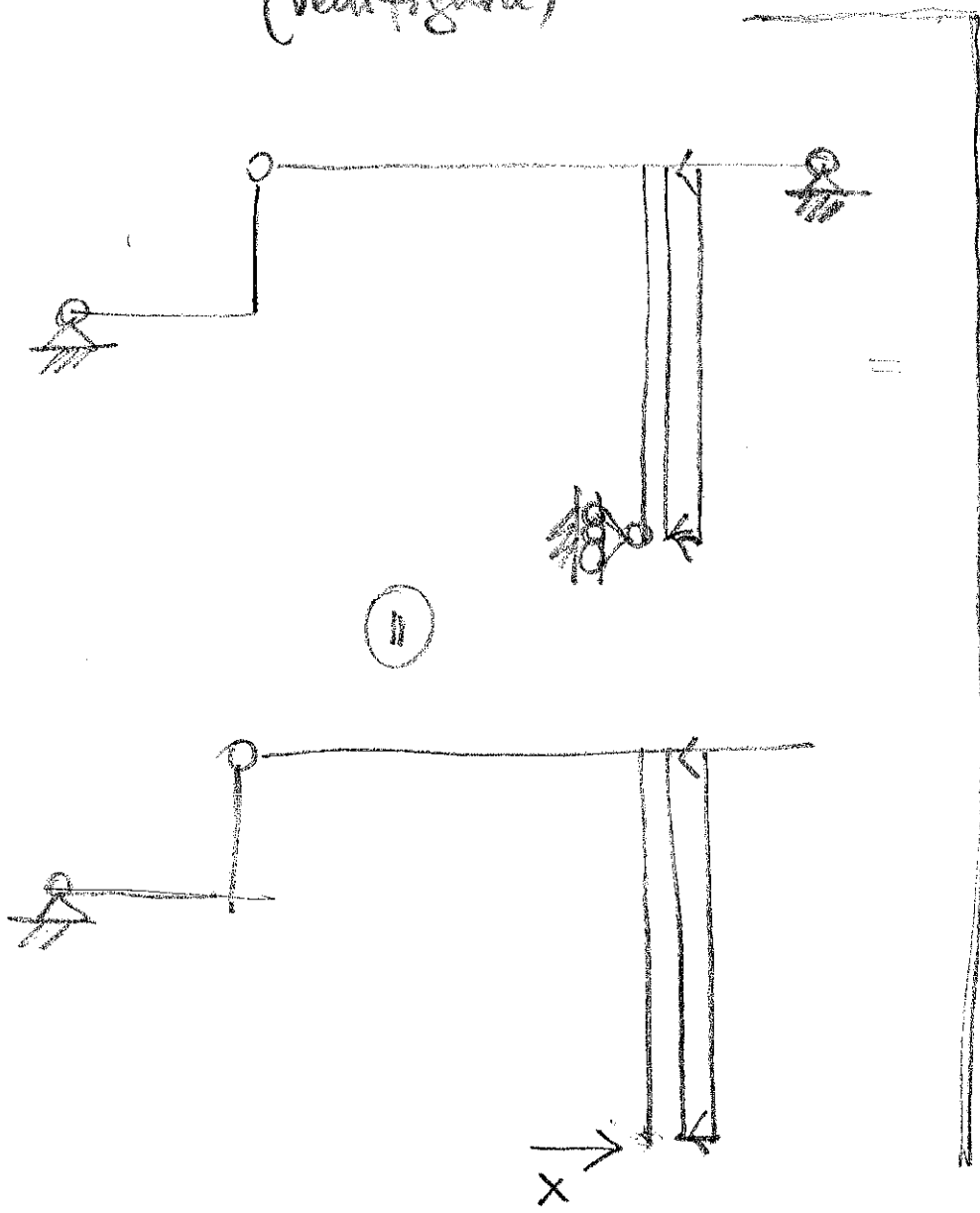
$$R(D) \frac{9}{2} = 1 + R(A) \rightarrow R(D) = \frac{2}{5}$$



simplificazioni
NB In tutti i tratti
 lineari il
 mom. simm. coincide
 con il mom. asim.
 $\Rightarrow \int M_1 M_0 = \frac{4l}{3} \frac{M_1}{2} \frac{M_0}{2}$

$$\begin{aligned}
 v(B) &= \int_{\text{struttura}} M_1 \frac{M_0}{EJ} = \underbrace{\frac{4}{3EJ} \frac{l}{2} \frac{2/5ql^2}{2} \frac{2/5l}{2}}_{\text{tratto A-A''}} + \underbrace{\frac{4}{3EJ} \frac{l}{2} \frac{2/5ql^2}{2} \frac{2/5l}{2}}_{\text{tratto A''-A'}} \\
 &+ \underbrace{\frac{4}{3EJ} \frac{2l}{2} \frac{6/5ql^2}{2} \frac{6/5l}{2}}_{\text{tratto A'-D'}} + \underbrace{\frac{4}{3EJ} l \frac{4/5ql^2}{2} \frac{4/5l}{2}}_{\text{tratto D'-D}} \\
 &+ \underbrace{\frac{4}{3EJ} \frac{2l}{2} \frac{2ql^2}{2} \frac{2l}{2} - \frac{2}{3EJ} \frac{2l}{8} \frac{q(2l)^2}{2} \cdot \frac{2l}{2}}_{\text{tratto D'-B}} \\
 &= \frac{ql^4}{EJ} \left(2 \frac{4}{3} \frac{l}{2} \frac{ql^3}{5^2} + \frac{4}{3} \frac{3}{2} \frac{l}{4} \frac{6^2}{5^2} ql^3 + \frac{4}{3} \frac{4}{5^2} ql^3 - \frac{2}{3} ql^4 \right) \\
 &= \frac{ql^4}{EJ} \frac{8 + 3 \times 6^2 + 16 \times 2 + 8 \times 2 \times 5^2 - 2 \times 2 \times 5^2}{6 \cdot 25} = \frac{224}{75} \frac{ql^4}{EJ}
 \end{aligned}$$

NB se lo schema reale è in realtà il risultato di uno schema iperstatico con X in corrispondenza dello spostam. orizzontale in B .
(vedi figura)



allora

$$M_x = -XM_1$$

è il diagramma dello schema virtuale (1) con X al posto della forza unitaria.

La sovrapposibilità degli effetti ammette quindi come momento complessivo della struttura iperstatica

$$M = M_0 + M_x = M_0 - XM_1$$

e quindi anche lo spostamento è

$$v(B) = v_0(B) - Xv_1(B)$$

Lo spostam. della struttura iperstatica deve essere per ragioni cinematiche nullo, cioè

spostam. calcolato prima con carico su struttura isostatica

$$0 = v(B) = \underbrace{\int_{\text{struttura}} M_1 \frac{M_0}{EJ}}_{v_0(B)} - X \underbrace{\int_{\text{struttura}} M_1 \frac{M_1}{EJ}}_{v_1(B)}$$

(14)

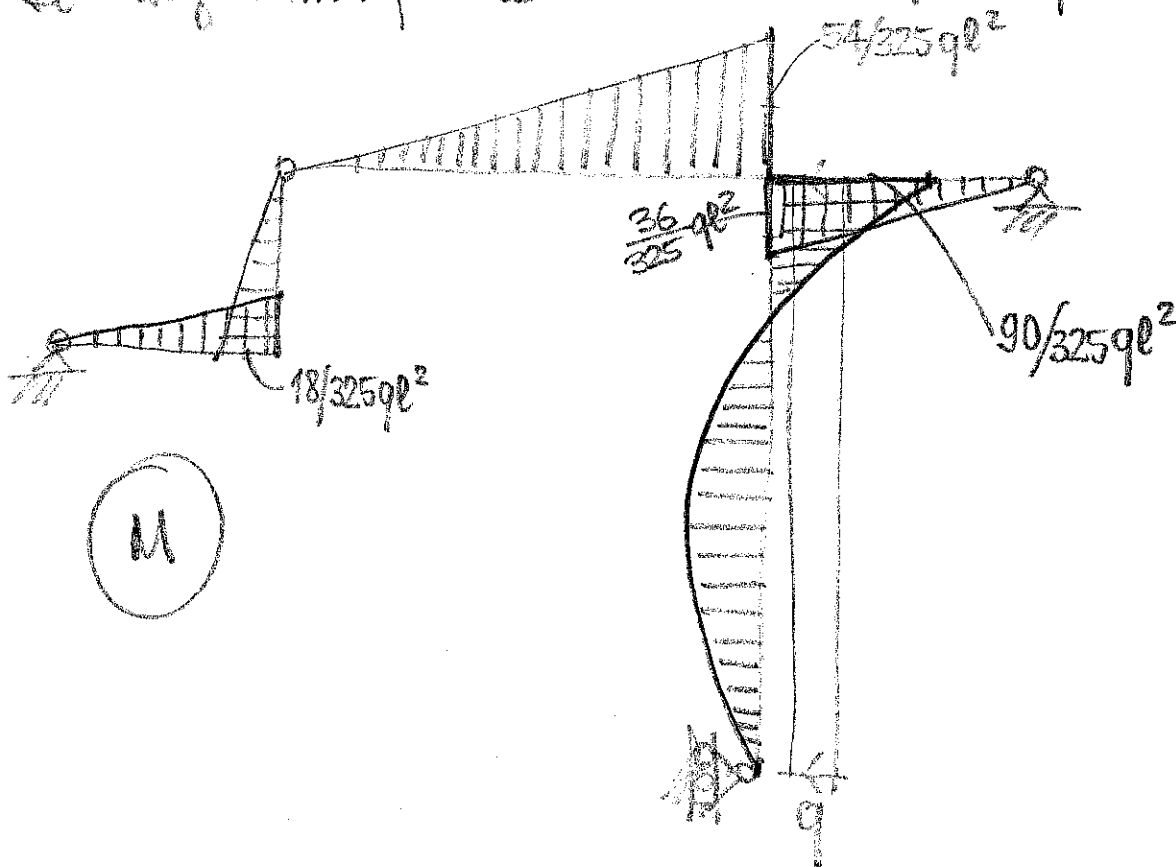
se si calcola $\int M_1 \frac{M_1}{EI}$ come fatto in precedenza
(si veda il diagramma M_1 a pag. 11) si ha

$$\Delta v_1(B) = \frac{l}{3EI} \left(\frac{2}{5}l \frac{2}{5}l + \frac{2}{5}l \frac{2}{5}l + \frac{6}{5}l \frac{6}{5}l + \frac{4}{5}l \frac{4}{5}l + 2l \cdot 2l \right)$$

$$= \frac{l^3}{75EI} (4 + 4 + 36 + 16 + 200) = \frac{260l^3}{75EI}$$

$$\Rightarrow X = \frac{224}{75} \frac{ql^4}{EI} \frac{75EI}{260l^3} = \frac{56}{65} ql$$

Il diagramma finale $M = M_0 - XM_1$ è quindi



$$- \frac{2}{5}l \cdot \frac{56}{65} ql + \frac{2}{5}ql^2 = \frac{2 \cdot 9}{325} ql^2 \dots$$

$$- 2l \frac{56}{65} ql + 2ql^2 = \frac{2 \cdot 9}{65} ql^2 \equiv \frac{10 \cdot 9}{325} ql^2$$